



## DANIËL VELDMAN

We consider the aluminum rod in Figure 1 with a length of L = 0.3 [m], a cross sectional area of  $A_{\rm cs} = 0.01$  [m<sup>2</sup>], and a thermal conductivity of k = 237 [W/m/K]. At five locations  $x_{{\rm meas},i} = (i-1)\frac{L}{4}$  ( $i \in \{1, 2, 3, 4, 5\}$ ) along the rod, temperature sensors are installed. Our aim is to reconstruct the heat load applied to the rod based on the measured temperatures  $\bar{T}_{{\rm meas},i}$  at these five locations.



FIGURE 1. The considered aluminum rod

We reconstruct the applied heat load by minimizing the functional

$$\mathcal{J}(Q) = \frac{1}{2} \sum_{i=1}^{5} (T(x_{\text{meas},i}) - \bar{T}_{\text{meas},i})^2 + \frac{w}{2} \int_0^L (Q(x))^2 \, \mathrm{d}x,$$

where w > 0 is a weight and T(x) is the steady-state temperature field resulting from the heat load Q(x) which satisfies

$$kA_{\rm cs}\frac{\mathrm{d}^2T}{\mathrm{d}x^2}(x) + Q(x) = 0, \qquad kA_{\rm cs}\frac{\mathrm{d}T}{\mathrm{d}x}(0) = hT(0), \qquad -kA_{\rm cs}\frac{\mathrm{d}T}{\mathrm{d}x}(L) = hT(L).$$

A finite element discretization of this problem takes the form

$$\begin{split} J(\mathbf{u}) &= \frac{1}{2} \mathbf{e}_{\text{meas}}^{\top} \mathbf{e}_{\text{meas}} + \frac{w}{2} \mathbf{u}^{\top} \mathbf{E} \mathbf{u}, \\ \mathbf{e}_{\text{meas}} &= \mathbf{E}_{\text{meas}} \mathbf{T} - \mathbf{T}_{\text{meas}}, \qquad \mathbf{A} \mathbf{T} + \mathbf{E} \mathbf{u} = \mathbf{0}, \end{split}$$

where **T** and **u** are vectors containing the nodal values of T(x) and Q(x),  $\mathbf{T}_{\text{meas}} = [\bar{T}_{\text{meas},1}, \bar{T}_{\text{meas},2}, \bar{T}_{\text{meas},3}, \bar{T}_{\text{meas},4}, \bar{T}_{\text{meas},5}]^{\top}$  and the 5 × N-matrix  $\mathbf{E}_{\text{meas}}$  (where N is the number of nodes) selects the nodal temperatures at the location of the temperature sensors. The matrices  $\mathbf{E}$ ,  $\mathbf{E}_{\text{meas}}$ , and  $\mathbf{A}$  for a FE model with M = 100 elements (and N = 101 nodes) are given in the file rod\_model.mat. This file also contains the vector  $\mathbf{T}_{\text{meas}}$  with the measured temperature values.

a. (2pts) Eliminate  $\mathbf{e}_{\text{meas}}$  and  $\mathbf{T}$  from the given expression of the discretized functional  $J(\mathbf{u})$ . Use the obtained expression to give explicit expressions for the Jacobian  $\partial J/\partial \mathbf{u}$ , the gradient  $\nabla J$  w.r.t. the standard Euclidean inner product, and the gradient  $\nabla J$  w.r.t. the weighted inner product based on the weighting matrix  $\mathbf{W} = \mathbf{E}$ .

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b. (4pts) Implement the basic gradient descent algorithm given at the end of lecture\_week9. Terminate the algorithm when the relative change in cost function and the relative change in **u** are below  $tol = 10^{-3}$ . Use  $w = 10^{-6}$ , an initial step size  $\beta_0 = 100$ , and the gradient w.r.t. to the weighted inner product with  $\mathbf{W} = \mathbf{E}$ .

Hint: You can use the file Week9\_exerciseb as a starting point.

- c. (2pts) Vary the weight w and explain what trend you observe in the obtained solutions. How does the choice of w influence the number of required iterations?
- d. (2pts) Replace the gradient computed w.r.t. the weighted inner product with the gradient computed w.r.t. the standard innerproduct. What do you observe in the obtained optimal solution?

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