

Controllability of Nodal Profile for a Network of Vibrating Strings

Yue WANG

Mini-WORKSHOP on Hyperbolic Problems, Erlangen, Oct. 2020



yue.wang@fau.de

- 1 Introduction
 - Nodal Control Problems: Motivation by application
 - State of the art
- 2 Network of Vibrating Strings
 - Problem Description: Star-shaped network
 - Constructive Method
 - Main Result: Exact Controllability of Nodal Profile
 - Remarks
- 3 Controllability of Nodal Profile in Hilbert Space. Duality Method.
 - Control Operator in Hilbert Space
 - Duality Method: duality of controllability and observability

Outline

- 1 Introduction
 - Nodal Control Problems: Motivation by application
 - State of the art
- 2 Network of Vibrating Strings
 - Problem Description: Star-shaped network
 - Constructive Method
 - Main Result: Exact Controllability of Nodal Profile
 - Remarks
- 3 Controllability of Nodal Profile in Hilbert Space. Duality Method.
 - Control Operator in Hilbert Space
 - Duality Method: duality of controllability and observability

Nodal Control Problems: Motivation by application

2010, 2014. M. Gugat, etc.

- The coupling of gas pipes.



Figure: Illustration of the control of a compressor station with two pipes. The first pipe corresponds to the supplier and the second to the customer.

Nodal Control Problems: Motivation by application

2010, 2014. M. Gugat, etc.

- The coupling of gas pipes.
- One dimensional isothermal Euler equations.

For a single pipe,

$$\rho_t + q_x = 0,$$
$$q_t + \left(\frac{q^2}{\rho} + a^2 \rho \right)_x = -f_g \frac{q|q|}{2D\rho},$$

$\rho(t, x)$: the density of the gas.

$q(t, x)$: the flux in the pipe.

$p = a^2 \rho$: the pressure of the flow.

Nodal Control Problems: Motivation by application

2010, 2014. M. Gugat, etc.

- The coupling of gas pipes.
- One dimensional isothermal Euler equations.
- Nodal Controls.

For a single pipe,

$$\begin{aligned} \rho_t + q_x &= 0, \\ q_t + \left(\frac{q^2}{\rho} + a^2 \rho \right)_x &= -f_g \frac{q|q|}{2D\rho}, \end{aligned}$$

The dynamics of the compressor :

$$\begin{aligned} q^{(1)}(t, 0) &= q^{(2)}(t, 0), \\ u(t) &= q^{(2)}(t, 0) \left(\left(\frac{\rho^{(2)}(t, 0)}{\rho^{(1)}(t, 0)} \right)^{\kappa} - 1 \right), \end{aligned}$$

$u(t)$: the nodal control.

⁰Ehrhardt K, Steinbach M. Nonlinear gas optimization in gas networks. In Modeling, Simulation and Optimization of Complex Processes, Bock HG, Kostina E, Pu HX, Rannacher R (eds). Springer: Berlin, 2005.

Nodal Control Problems: Motivation by application

2010, 2014. M. Gugat, etc.

- The coupling of gas pipes.
- One dimensional isothermal Euler equations.
- Nodal Controls.
- Exact controllability of boundary traces.

(P): Given finite time $T_0 > \bar{T} > 0$, we choose $t^* \in (\bar{T}, T_0)$ such that after the finite time t^* ,
can we find $u \in C^1([0, T_0])$ such that system has a classical solution that satisfies the given customer demand in density and flux by

$$(\rho^{(2)}, q^{(2)}) \Big|_{x=L_2} = (\rho_B(t), q_B(t)) \quad \text{for all } t \in [t^*, T_0],$$

where ρ_B and q_B are given C^1 functions?

Exact controllability of nodal profiles

Main Result: [2011. M. Gugat, etc.]¹

In a C^1 -neighborhood of the stationary state $(\bar{\rho}^{(i)}, \bar{q}^{(i)})$ with $i = 1, 2$, we can construct a continuously differentiable compressor control u such that the demand is fulfilled exactly for all $t \in [t^*, T_0]$ with the lower bound of t^* greater than

$$\bar{T} = \max \left\{ \frac{L_2}{|\lambda_i^{(2)}(\bar{\rho}^{(2)}, \bar{q}^{(2)})|} \right\}, \quad i = 1, 2. \quad (1)$$

¹M. Gugat, M. Herty, V. Schleper. Flow control in gas networks: exact controllability to a given demand, Math. Methods Appl. Sci., 34(7):745-757, 2011.

State of the art

- 2010, 2014. **M. Gugat, etc.** The coupling of gas pipes, one dimensional isothermal Euler equations, nodal controls.
- 2010. **Tatsien LI.** ²1-D first order quasilinear hyperbolic systems.

$$\mathbf{u}_t + A(\mathbf{u})\mathbf{u}_x = \mathbf{F}(\mathbf{u}),$$

where $\mathbf{u} = (u_1, \dots, u_n)^T$, $A(\mathbf{u}) = (a_{ij}(u))_{n \times n}$, $F(\mathbf{u}) = (f_1(u), \dots, f_n(u))^T$.

- 2010-2016. **Tatsien LI, Ke WANG, Qilong GU.** A complete theory on 1-D wave equations and unsteady flows on networks (without loops).
- 2019. **Yue Wang, Tatsien LI.** EBC of partial nodal profile.
- 2019. **Libin Wang, Ke Wang.** Asymptotic stability of the exact boundary controllability of nodal profile for 1-D quasilinear wave equations.

Remark

- Semi-global classical solution for nonlinear case.
- Local result in the C^1 (or C^2) neighborhood of the stationary state.

²Tatsien Li, Exact boundary controllability of nodal profile for quasilinear hyperbolic systems, Math. Methods Appl. Sci. 33(17), 2101–2106, 2010.   

Outline

- 1 Introduction
 - Nodal Control Problems: Motivation by application
 - State of the art
- 2 Network of Vibrating Strings
 - Problem Description: Star-shaped network
 - Constructive Method
 - Main Result: Exact Controllability of Nodal Profile
 - Remarks
- 3 Controllability of Nodal Profile in Hilbert Space. Duality Method.
 - Control Operator in Hilbert Space
 - Duality Method: duality of controllability and observability

Definition

Definition 1: Degree

The **degree** $d(\geq 1)$ of the node E refers to the number of strings connected to it.
 If $d = 1$, the node is **simple node**;
 if $d > 1$, the node is **multiple node**.



Figure: Simple node $d = 1$

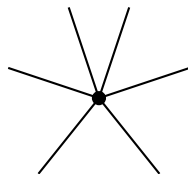


Figure: Multiple node $d > 1$

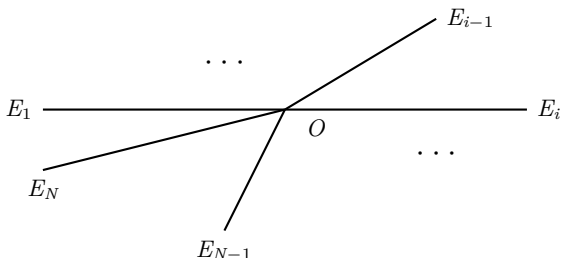
Star-shaped network

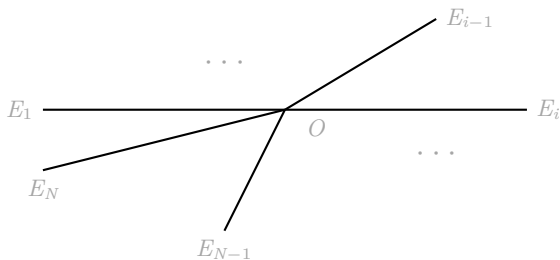
Consider a star-shaped network composed of N strings with a joint node O of degree N .

Let the coordinate of O be $x = 0$.

For $i = 1, \dots, N$, E_i is the simple node of the i -th string with length L_i .

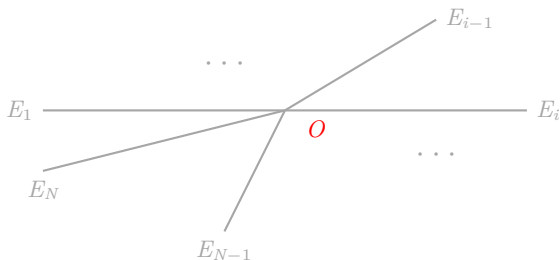
The i -th string can be parameterized as $x \in [0, L_i]$.





$$y_{tt}^i - a_i^2 y_{xx}^i = 0, \quad 0 < x < L_i, t > 0 \quad (i = 1, \dots, N), \quad (2)$$

where y^i , the transversal displacement of the i -th string, is unknown C^2 function of (t, x) and $a_i > 0$ is given positive constant for each $i = 1, \dots, N$.



At the multiple node O , we prescribe N transmission conditions:

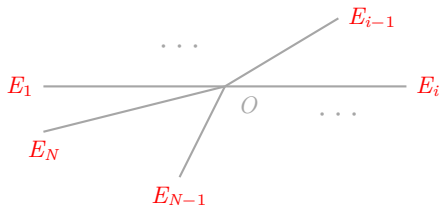
1 stress interface condition

$$\sum_{i=1}^N a_i^2 y_x^i = u_0(t) \quad (3)$$

and $(N-1)$ displacement interface conditions

$$y^i = y^1 \quad (i = 2, \dots, N), \quad (4)$$

where $u_0(t)$ is a given function at O or a control function to be determined.



For $i = 1, \dots, N$, at each simple node E_i , we prescribe any **one** of the following boundary conditions:

$$x = L_i : \quad y^i = u_i(t) \quad (\text{Dirichlet type}), \quad (5a)$$

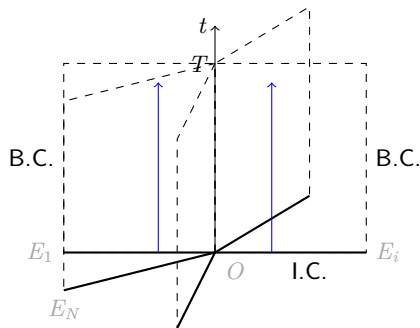
$$x = L_i : \quad y_x^i = u_i(t) \quad (\text{Neumann type}), \quad (5b)$$

$$x = L_i : \quad y_x^i + \theta_i y^i = u_i(t), \quad (\text{Robin type}), \quad (5c)$$

$$x = L_i : \quad y_x^i + \gamma_i y_t^i = u_i(t), \quad (\text{Dissipative type}), \quad (5d)$$

where θ_i and γ_i are given positive constants, $u_i \in C^2$ (for (6a)) or $u_i \in C^1$ (for (6b)-(6d)) is a given boundary function or a control function to be determined.

Wellposedness



Let $T > 0$. With any given initial data

$$t = 0 : (y^i, y_t^i) = (\phi_i, \psi_i), \quad 0 \leq x \leq L_i (i = 1, \dots, N), \quad (6)$$

where $(\phi_i, \psi_i) \in C^2[0, L_i] \times C^1[0, L_i]$ compatible to the boundary data, the mixed initial-boundary valued problem (2)-(6) admits a unique piece-wise C^2 solution y on the domain $\mathcal{R}(T) = \cup_{i=1}^N \{(t, x) | 0 \leq t \leq T, 0 \leq x \leq L_i\}$.

Exact Control Problem of Nodal Profile

Definition 2 & Notations

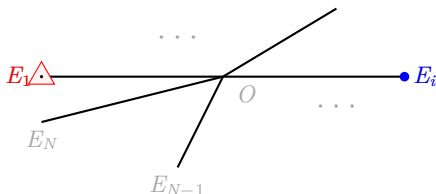
(Charged node):

—● with given (partial or total) nodal profiles.

(Controlled node):

—△ with boundary control to be determined.

(At most one boundary control on each node).



(P): Given finite time $T > \bar{T} > 0$.
Can we find one

Exact Control Problem of Nodal Profile

Definition 2 & Notations

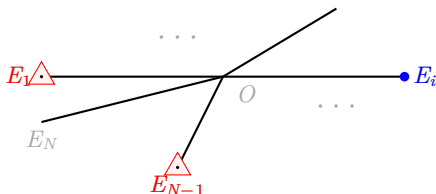
(Charged node):

—● with given (partial or total) nodal profiles.

(Controlled node):

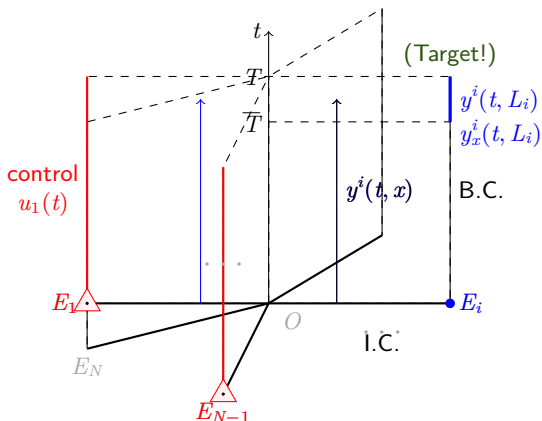
—△ with boundary control to be determined.

(At most one boundary control on each node).



(P): Given finite time $T > \bar{T} > 0$.
Can we find one or more boundary controls $w^j \in C^1[0, T]$ (or $\in C^2[0, T]$)

Exact Control Problem of Nodal Profile



(P): Given finite time $T > \bar{T} > 0$. Can we find one or more boundary controls $w^j \in C^1[0, T]$ (or $\in C^2[0, T]$) to drive the boundary trace of the solution to system (2)-(6) to desired values at certain node E_i after the given finite time \bar{T} :

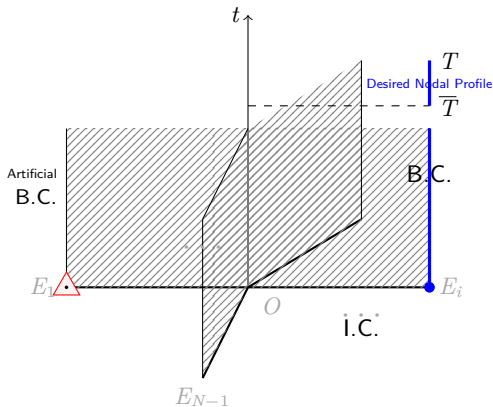
$$y^i(t, L_i) = \tilde{y}_i(t), \quad \bar{T} \leq t \leq T,$$

or

$$y_x^i(t, L_i) = \bar{y}_i(t), \quad \bar{T} \leq t \leq T,$$

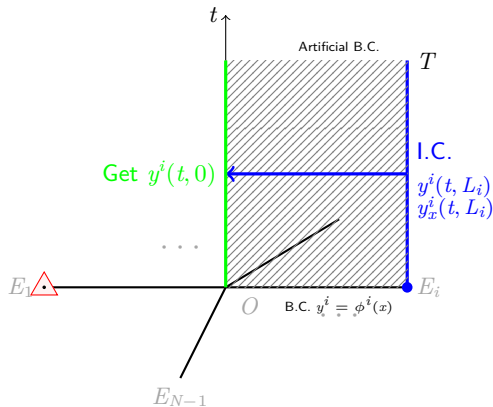
where $\tilde{y}_i(t) \in C^2[\bar{T}, T]$ and $\bar{y}_i(t) \in C^1[\bar{T}, T]$ are given profile as functions of time and compatible to the B.C.

Exact Controllability of Nodal Profile: Constructive Method



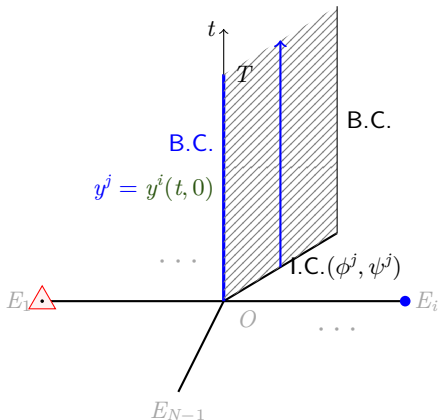
- 1 Forward problem on the whole network.
- 2 Connect the trace. (not unique)

Exact Controllability of Nodal Profile: Constructive Method



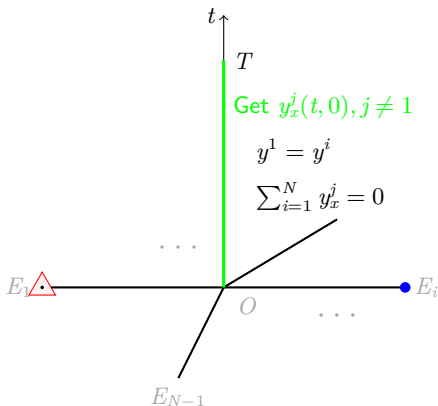
- 1 Forward problem on the whole network.
- 2 Connect the trace. (not unique)
- 3 Change the role of t and x . Sidewise problem from the charged node.

Exact Controllability of Nodal Profile: Constructive Method



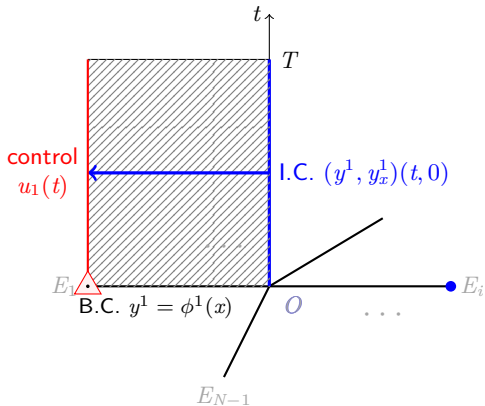
- 1 Forward problem on the whole network.
- 2 Connect the trace. (not unique)
- 3 Change the role of t and x . Sidewise problem from the charged node.
- 4 Solve forward problem on uncontrolled strings.

Exact Controllability of Nodal Profile: Constructive Method



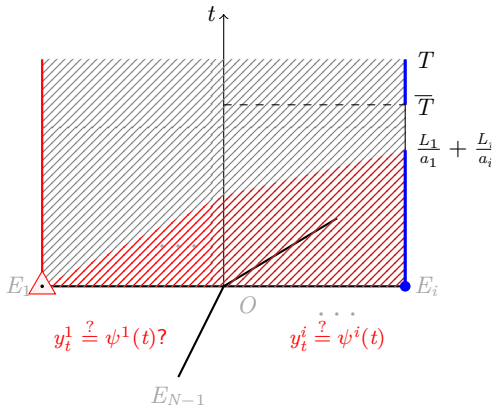
- 1 Forward problem on the whole network.
- 2 Connect the trace. (not unique)
- 3 Change the role of t and x . Sidewise problem from the charged node.
- 4 Solve forward problem on uncontrolled strings.

Exact Controllability of Nodal Profile: Constructive Method



- 1 Forward problem on the whole network.
- 2 Connect the trace. (not unique)
- 3 Change the role of t and x . Sidewise problem from the charged node.
- 4 Solve forward problem on uncontrolled strings.
- 5 Solve sidewise problem from $x = 0$ to the controlled end
- 6 Determine the boundary control by the trace.

Exact Controllability of Nodal Profile: Constructive Method



- 1 Forward problem on the whole network.
- 2 Connect the trace. (not unique)
- 3 Change the role of t and x . Sidewise problem from the charged node.
- 4 Solve forward problem on uncontrolled strings.
- 5 Solve sidewise problem from $x = 0$ to the controlled end
- 6 Determine the boundary control by the trace.
- 7 Verify I.C.; Uniqueness

Main Result: EBC of Nodal Profile

Theorem 1³

For one charged node with given nodal profiles, there exist

- a finite time \bar{T} (called controllability time),
- and $N(C)$ boundary controls

such that the system (2)-(5) is **exact controllable of nodal profile** after \bar{T} .

Furthermore, the minimum number of desired controls

$$N(C) = \text{Freedom Degree of the charged node.}$$

Definition 3

Freedom Degree of the charged node is

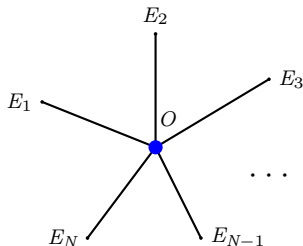
The number of given nodal profiles – The number of related constraints ,

where the **constraints** refers to given boundary conditions or interface conditions that must be fitted for the given nodal profiles on the charged node.

³Yue Wang, Tatsien Li. Exact Boundary Controllability of Partial Nodal Profile for Wave Equations, Submitted, 2019. 

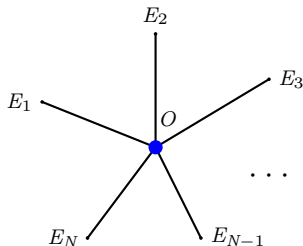
Case 1: Multiple node charged with N displacement nodal profiles

- Target: $(y^1, \dots, y^N)(t, 0) = (\tilde{y}^1(t), \dots, \tilde{y}^N(t)), t \in [\overline{T}, T]$.



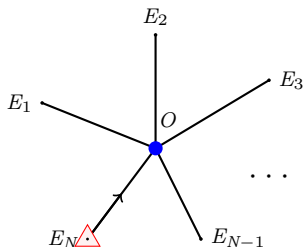
Case 1: Multiple node charged with N displacement nodal profiles

- Target: $(y^1, \dots, y^N)(t, 0) = (\tilde{y}^1(t), \dots, \tilde{y}^N(t)), t \in [\overline{T}, T]$.
- $(N - 1)$ interface conditions $y^j = y^1, j \neq 1$.
- Freedom Degree: $N(O) = 1$.



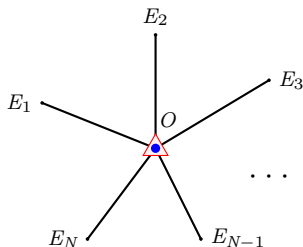
Case 1: Multiple node charged with N displacement nodal profiles

- Target: $(y^1, \dots, y^N)(t, 0) = (\tilde{y}^1(t), \dots, \tilde{y}^N(t)), t \in [\bar{T}, T]$.
- $(N - 1)$ interface conditions $y^j = y^1, j \neq 1$.
- Freedom Degree: $N(O) = 1$.
- Number of desired controls: **1**.
- simple node:
controllability time: $\bar{T} > \frac{L_N}{a_N}$.



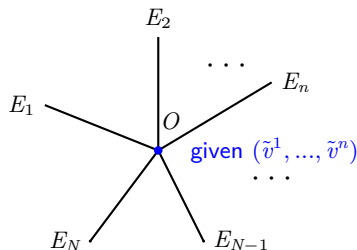
Case 1: Multiple node charged with N displacement nodal profiles

- Target: $(y^1, \dots, y^N)(t, 0) = (\tilde{y}^1(t), \dots, \tilde{y}^N(t)), t \in [\bar{T}, T]$.
- $(N - 1)$ interface conditions $y^j = y^1, j \neq 1$.
- Freedom Degree: $N(O) = 1$.
- Number of desired controls: **1**.
 - simple node:
controllability time: $\bar{T} > \frac{L_N}{a_N}$.
 - multiple O :
controllability time: $\bar{T} > 0$.



Case 2: Multiple node charged with partial nodal profiles

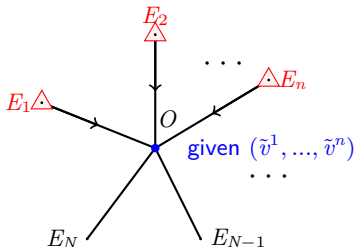
- Target: $(y_x^1, \dots, y_x^n)(t, 0) = (\tilde{y}^1(t), \dots, \tilde{y}^n(t)), t \in [\bar{T}, T]$.
- 1 transmission condition $\sum_i^N a^i y_x^i = 0$.
- If $n = N$, freedom Degree: $N(O) = N - 1$.



Case 2: Multiple node charged with partial nodal profiles

- Target: $(y_x^1, \dots, y_x^n)(t, 0) = (\tilde{y}^1(t), \dots, \tilde{y}^n(t)), t \in [\bar{T}, T]$.
- If $n < N$, freedom Degree: $N(O) = n$.
- Number of controls: n .
 - n simple nodes:

$$\bar{T} > \max_{1 \leq j \leq n} \frac{L_j}{a_j}.$$

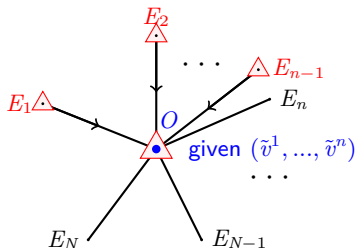


Case 2: Multiple node charged with partial nodal profiles

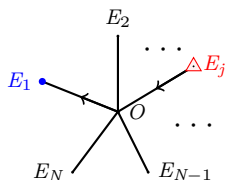
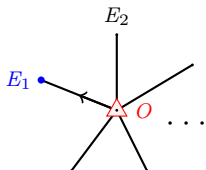
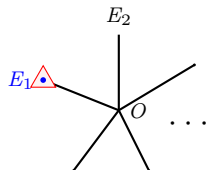
- Target: $(y_x^1, \dots, y_x^n)(t, 0) = (\tilde{y}^1(t), \dots, \tilde{y}^n(t)), t \in [\bar{T}, T]$.
- If $n < N$, freedom Degree: $N(O) = n$.
- Number of controls: n .
 - n simple nodes:

$$\bar{T} > \max_{1 \leq j \leq n} \frac{L_j}{a_j}.$$
 - multiple O and $n - 1$ simple nodes:

$$\bar{T} > \max_{1 \leq j \leq n-1} \frac{L_j}{a_j}.$$



Case 3: Simple node charged with partial nodal profiles

(a) Simple controlled node $E_j (j \neq 1)$ (b) Multiple controlled node O 

(c) In-situ controlled node

The charged node E_1 is always of freedom degree 1.

Fig.	Charged node	Controlled node	Controllability Time \bar{T}
(a)	E_1	$E_j (j \neq 1)$	$\bar{T} > \frac{L_1}{a_1} + \frac{L_j}{a_j}$
(b)	E_1	O	$\bar{T} > \frac{L_1}{a_1}$
(c)	E_1	E_1 (in-situ)	$\bar{T} > 0$

Summary

In summary, we find that for one charged node,

- Minimum number of desired controls = Freedom degree of the charged node.
- Controllability time = the transmission time from the controlled node to the charged node.

The proof is based on

- Existence and Uniqueness Theory on global piecewise C^2 solution to the mixed problem on the network.
- Method: Constructive Method.

Some Remarks

Remark1: Planar Tree-like Network

The previous results can be generalized to the tree-like network satisfying some requirements of number and position of charged nodes and controlled nodes.

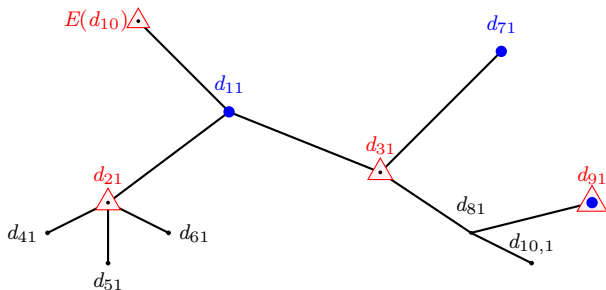


Figure: Charged nodes d_{11} , d_{71} and d_{91} , of which the degree of freedom is 2, 1 and 1.

Some Remarks

Remark1: Planar Tree-like Network

The previous results can be generalized to the tree-like network satisfying some requirements of number and position of charged nodes and controlled nodes.

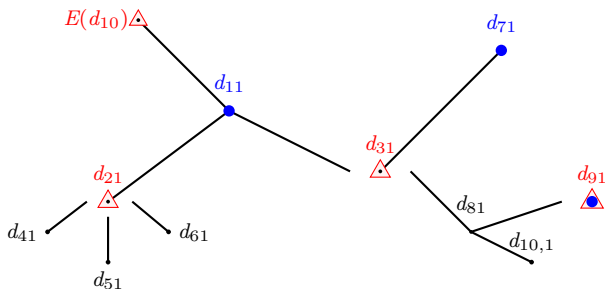


Figure: Split nodes d_{21} , d_{31} and d_{91} .

Some Remarks

Remark2: Quasilinear Case

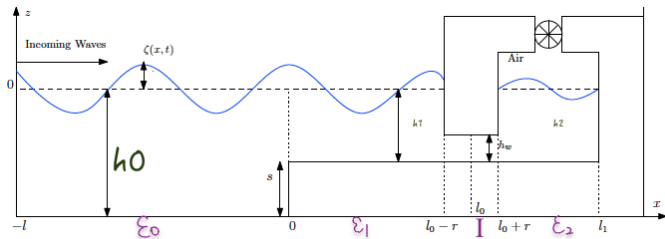
The previous results can be generalized to the corresponding quasilinear case .

$$u_{tt}^i - (K^i(u^i, u_x^i))_x = F^i(u^i, u_x^i, u_t^i), \quad t \geq 0, d_{i0} \leq x \leq d_{i1}, \quad (7)$$

- In C^2 neighborhood of stationary state.
- Semi-global C^2 solution with C^2 norm.
- Construct a solution.

Remark3: Harvesting Model

This method can be used to other one-dimension hyperbolic system in the framework of classical solutions.



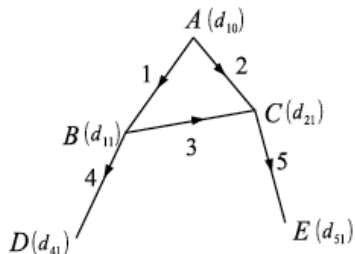
1D nonlinear shallow water equations ⁴.

$$\begin{cases} \partial_t \zeta + \partial_x q = 0, \\ \partial_t q + \partial_x \left(\frac{q^2}{h} \right) + gh \partial_x \zeta = 0 \end{cases} \quad (8)$$

⁴E. Bocchi, J. He and G. Vergara-Hermosilla, Modelling and simulation of a wave energy converter, ESAIM: PROCEEDINGS AND SURVEYS, 1-10, 2019.

Remark4: Saint-Venant system on a network with loops

- The Saint-Venant system has **no** exact boundary controllability on a network with loops in general. [1994, J.E. Lagnese, G. Leugering, E. J. P. G. Schmidt].
- BUT it is **possible** to get the exact boundary controllability of nodal profile for Saint-Venant system on certain networks with loops. [2019, Kaili Zhuang, G. Leugering, Tatsien Li].



Outline

- 1 Introduction
 - Nodal Control Problems: Motivation by application
 - State of the art
- 2 Network of Vibrating Strings
 - Problem Description: Star-shaped network
 - Constructive Method
 - Main Result: Exact Controllability of Nodal Profile
 - Remarks
- 3 Controllability of Nodal Profile in Hilbert Space. Duality Method.
 - Control Operator in Hilbert Space
 - Duality Method: duality of controllability and observability

Introduction

- Working space: Hilbert space.
- Linear control problem of nodal profile.
- Duality method: **duality between controllability and observability** .
- **observability inequalities**.
- Exact controllability problem (Final data at T): J.-L. Lions⁵, E. Zuazua⁶, J. M. Coron.⁷.

⁵J. -L. Lions, Contrôlabilité Exacte, Perturbations et Stabilisation de Systèmes Distribués, Vol. I, Masson, (1988).

⁶E. Zuazua, Exact controllability for semilinear wave equations in one space dimension, Annales de l'I. H. P., section C, tome 10, no 1 (1993), p. 109-129.

⁷J. M. Coron, Control and Nonlinearity, Mathematical Surveys and Monographs Vol.136, American Mathematical Society, 2007. 

Star-shaped Network: The Three String Network with Two Controlled Nodes

We consider the simplest non-trivial network of strings that cannot be reduced to a single string: the three string network.

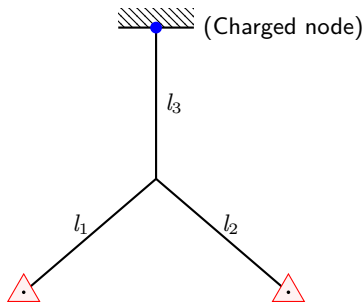


Figure: Three string Network with two controls

Equations of Motion of the Network

Let T, l_1, l_2, l_3 be positive numbers. We consider the following non-homogeneous system

$$\left\{ \begin{array}{l} y_{tt}^i - y_{xx}^i = 0, \quad (t, x) \in (0, T) \times (0, l_i), \quad i = 1, 2, 3, \\ x = 0 : y^1(t, 0) = y^2(t, 0) = y^3(t, 0), \quad t \in (0, T), \\ \quad y_x^0(t, 0) + y_x^1(t, 0) + y_x^2(t, 0) = 0, \quad t \in (0, T), \\ x = l_3 : y^3(t, l_3) = 0, \quad t \in (0, T), \\ x = l_i : y_x^i(t, l_i) = u^i(t), \quad t \in (0, T), \quad i = 1, 2, \end{array} \right. \quad (9)$$

with any given initial data

$$(y^i, y_t^i)(0, x) = (y_0^i, y_1^i)(x), \quad 0 \leq x \leq l_i, \quad i = 1, 2, 3, \quad (10)$$

which models the vibrations of a network formed by three elastic strings with the lengths l_1, l_2, l_3 coupled at one of their extremes at $x = 0$. The functions

$y^i = y^i(t, x) : [0, l_i] \rightarrow \mathbb{R}, i = 1, 2, 3$, represent the transversal displacements of the strings. Here we take Neumann controls u^1 and u^2 .

We introduce the working spaces

$$V = \left\{ \psi \in \prod_{i=1}^3 H^1(0, l_i) \mid \psi^1(0) = \psi^2(0) = \psi^3(0), \psi^3(l_3) = 0 \right\}, \quad (11)$$

$$H = \prod_{i=1}^3 L^2(0, l_i)$$

with the inner product

$$(\vec{\phi}, \vec{\psi})_V = \sum_{i=1}^3 \frac{1}{2} \int_0^{l_i} \phi_x^i \cdot \psi_x^i dx, \quad (12)$$

$$(\vec{\phi}, \vec{\psi})_H = \sum_{i=1}^3 \frac{1}{2} \int_0^{l_i} \phi^i \cdot \psi^i dx.$$

In the following, $\vec{y} = (y^1, y^2, y^3)$, and \vec{y}_0, \vec{y}_1 denotes the corresponding initial displacement and velocity, respectively.

Theorem 2.1 (Wellposedness)

For any given initial data $(\vec{y}_0, \vec{y}_1) \in V \times H$ and boundary functions $u^1, u^2 \in L^2(0, T)$, the corresponding compatibility conditions are satisfied at the nodes $(0, l_1)$ and $(0, l_2)$, then system (9)-(10) admits a unique solution ⁸:

$$\vec{y} \in C([0, T]; V) \cap C^1([0, T]; H). \quad (13)$$

Furthermore, we can get a Neumann trace hidden regularity result at the end $x = l_3$ with homogenous Dirichlet boundary condition that: the map

$$\{\vec{y}_0, \vec{y}_1\} \mapsto y_x^3|_{x=l_3} : V \times H \rightarrow L^2(\{x = l_3\} \times (0, T)) \quad (14)$$

is continuous.

⁸J.E. Lagnese, G. Leugering, Schmidt, Modeling, Analysis and Control of Dynamic Elastic Multi-Link Structures, 1994

Boundary Control Problem of Nodal Profile

(P): Let $T > \bar{T} > 0$. For given desired profile function $\bar{y}_3(t) \in L^2(\bar{T}, T)$ to find boundary controls $u^1, u^2 \in L^2(0, T)$ so that

$$\mathcal{F}(u^1, u^2) = \bar{y}_3(t).$$

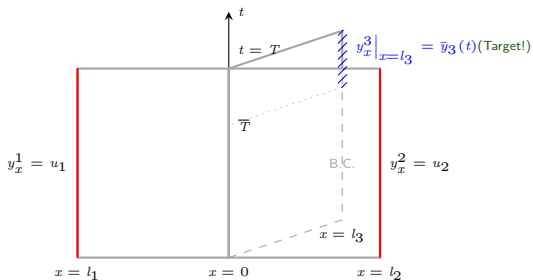


Figure: Control Problem: y -system

Control Operator

Step 1: Define a mapping to describe the control problem

For given $T > \bar{T} > 0$, define a mapping

$$\boxed{\begin{aligned} \mathcal{F} : U &\longrightarrow L^2(\bar{T}, T) \\ (u^1, u^2) &\mapsto y_x^3(t, l_3) \end{aligned}} \quad (15)$$

where $U = L^2(0, T) \times L^2(0, T)$, $y_x^3(t, l_3)$ is the Neumann trace at the end $x = l_3$ of the corresponding solution $\vec{y} \in C^0([0, T]; V) \cap C^1([0, T]; H)$ to the system (9) with null initial data $(\vec{y}_0, \vec{y}_1)(x) = (0, 0)$ and boundary controls u^1, u^2 at $x = l_1$ and $x = l_2$. Then

Definition 2.2 [Boundary Controllability of Nodal Profile]

The system (9) is controllable of nodal profile at charged node $x = l_3$ in time $t \in (\bar{T}, T)$ if the control operator \mathcal{F} is onto.

Main Result

Our main controllability result is

Theorem 2.3

Let

$$\bar{T} = l_3 + \max\{l_1, l_2\} \quad (16)$$

and $T > \bar{T}$. Then the system (9) is controllable of nodal profile at $x = l_3$ in time $t \in (\bar{T}, T)$.

Method: Duality between controllability and observability

Framework:

- Controllability for a linear control system

¹⁰Rudin, Functional Analysis, 1973, P97;

¹⁰Coron, Control and Nonlinearity, P35

Method: Duality between controllability and observability

Framework:

- Controllability for a linear control system
- \iff the surjectivity of a certain linear map \mathcal{F} from a Hilbert space H_1 to another Hilbert space H_2 .

¹⁰Rudin, Functional Analysis, 1973, P97;

¹⁰Coron, Control and Nonlinearity, P35

Method: Duality between controllability and observability

Framework:

- Controllability for a linear control system
- \iff the surjectivity of a certain linear map \mathcal{F} from a Hilbert space H_1 to another Hilbert space H_2 .
- \iff the existence of $c > 0$ such that

$$\|\mathcal{F}^*(x_2)\|_{H_1} \geq c\|x_2\|_{H_2}, \quad \forall x_2 \in H_2, \quad (17)$$

where $\mathcal{F}^* : H_2 \rightarrow H_1$ is the adjoint of \mathcal{F} . This inequality (17) is called the observability inequality. ⁹¹⁰

⁹Rudin, Functional Analysis, 1973, P97;

¹⁰Coron, Control and Nonlinearity, P35

Method: Duality between controllability and observability

Framework:

- Controllability for a linear control system
- \iff the surjectivity of a certain linear map \mathcal{F} from a Hilbert space H_1 to another Hilbert space H_2 .
- \iff the existence of $c > 0$ such that

$$\|\mathcal{F}^*(x_2)\|_{H_1} \geq c\|x_2\|_{H_2}, \quad \forall x_2 \in H_2, \quad (17)$$

where $\mathcal{F}^* : H_2 \rightarrow H_1$ is the adjoint of \mathcal{F} . This inequality (17) is called the observability inequality.⁹¹⁰

- So, we need to

¹⁰Rudin, Functional Analysis, 1973, P97;

¹⁰Coron, Control and Nonlinearity, P35

Method: Duality between controllability and observability

Framework:

- Controllability for a linear control system
- \iff the surjectivity of a certain linear map \mathcal{F} from a Hilbert space H_1 to another Hilbert space H_2 .
- \iff the existence of $c > 0$ such that

$$\|\mathcal{F}^*(x_2)\|_{H_1} \geq c\|x_2\|_{H_2}, \quad \forall x_2 \in H_2, \quad (17)$$

where $\mathcal{F}^* : H_2 \rightarrow H_1$ is the adjoint of \mathcal{F} . This inequality (17) is called the observability inequality.⁹¹⁰

- So, we need to
 - compute \mathcal{F}^*

¹⁰Rudin, Functional Analysis, 1973, P97;

¹⁰Coron, Control and Nonlinearity, P35

Method: Duality between controllability and observability

Framework:

- Controllability for a linear control system
- \iff the surjectivity of a certain linear map \mathcal{F} from a Hilbert space H_1 to another Hilbert space H_2 .
- \iff the existence of $c > 0$ such that

$$\|\mathcal{F}^*(x_2)\|_{H_1} \geq c\|x_2\|_{H_2}, \quad \forall x_2 \in H_2, \quad (17)$$

where $\mathcal{F}^* : H_2 \rightarrow H_1$ is the adjoint of \mathcal{F} . This inequality (17) is called the observability inequality. ⁹¹⁰

- So, we need to
 - compute \mathcal{F}^*
 - and then prove (17).

¹⁰Rudin, Functional Analysis, 1973, P97;

¹⁰Coron, Control and Nonlinearity, P35

Dual System; Observability

Step 2: Compute adjoint operator \mathcal{F}^* . We introduce the following adjoint system:

$$\left\{ \begin{array}{l} \phi_{tt}^i - \phi_{xx}^i = 0 \quad (i = 1, 2, 3), \\ x = 0 : \sum_{i=1}^3 \phi_x^i = 0, \\ \phi^1 = \phi^2 = \phi^3, \\ x = l_i : \phi_x^i = 0 \quad (i = 1, 2), \\ x = l_3 : \phi^3 = \begin{cases} 0, & t \in [0, \overline{T}], \\ \varphi_3(t), & t \in [\overline{T}, T], \end{cases} \\ t = T : (\phi^i, \phi_t^i) = (0, 0) \quad (i = 1, 2, 3), \end{array} \right. \quad (18)$$

where $\varphi_3(t) \in L^2(\overline{T}, T)$.

Lemma 2.4

\mathcal{F} is an onto mapping if and only if for the adjoint mapping \mathcal{F}^* , there exists a constant $c > 0$ such that

$$\|\mathcal{F}^*(\varphi_3)\|_U \geq c\|\varphi_3\|_{L^2[\overline{T}, T]}, \quad \forall \varphi_3 \in L^2(\overline{T}, T). \quad (19)$$

$$\boxed{\mathcal{F}^* : L^2(\overline{T}, T) \longrightarrow L^2(0, T) \times L^2(0, T)} \quad (20)$$

we are going to take a dense set in $H_0^1(\overline{T}, T) \subset L^2(\overline{T}, T)$ to define how \mathcal{F}^* operates., and prove the corresponding observability inequality. Then, by a classical density argument and extension by continuity, the definition and inequality can be extended to the whole space $L^2(\overline{T}, T)$.

Adjoint Operator

Lemma 2.5

\mathcal{F}^* , the adjoint operator of \mathcal{F} , is densely defined on $H_0^1(\bar{T}, T)$ as:

$$\mathcal{F}^*(-\varphi_3(t)) = (\phi^1(\cdot, l_1), \phi^2(t, l_2)) \quad \forall \varphi_3(t) \in H_0^1(\bar{T}, T),$$

where $(\phi^1(t, l_1), \phi^2(t, l_2))$ are the trajectories of the solution $\vec{\phi} := \vec{\phi}(t, x)$ to the adjoint system (18). Moreover, we have the following dual identity

$$\langle (u^1, u^2), (\phi^1(\cdot, l_1), \phi^2(\cdot, l_2)) \rangle_{L^2(0, T) \times L^2(0, T)} = \langle \mathcal{F}(u^1, u^2), -\varphi_3 \rangle_{L^2(\bar{T}, T)}. \quad (21)$$

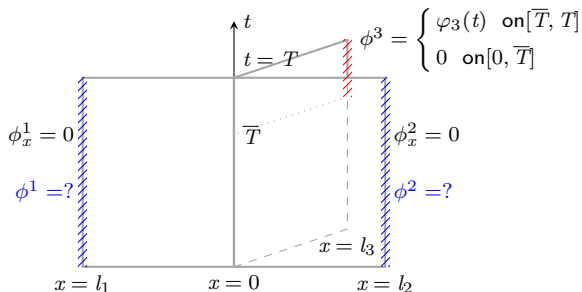
Observability Inequality

Theorem 2.6

Let $\bar{T} > l_3 + \max\{l_1, l_2\}$ and $T > \bar{T}$. There exists a constant $c > 0$, such that the observability inequality the adjoint problem (18) that

$$\|(\phi^1(\cdot, l_1), \phi^2(\cdot, l_2))\|_{L^2(0, T) \times L^2(0, T)} \geq c \|\varphi_3(\cdot)\|_{L^2(\bar{T}, T)}, \forall \varphi_3 \in H_0^1(\bar{T}, T). \quad (22)$$

So far, we shift the control problem of y -system (9) to the dual problem of ϕ -system (18)(shown in Fig.) .




Prove the Observability Inequality

Step3: The observability inequality. From the densely defined of \mathcal{F}^* , here we only prove the observability inequality for $\varphi_3 \in H_0^1(\overline{T}, T)$.

Two methods:

- the explicit solution of the adjoint problem (18), side-wise D' Alembert Formula¹¹. (Dáger, Zuazua)
- the multiplier method. (Alabau)

¹¹René Dáger, Enrique Zuazua. Wave Propagation, Observation and Control in 1–d Flexible Multi-Structures 

Proof of Observability Inequality

Step3.1(Backward Problem):

- Consider the backward mixed initial boundary value problem (18).

- \implies Unique solution

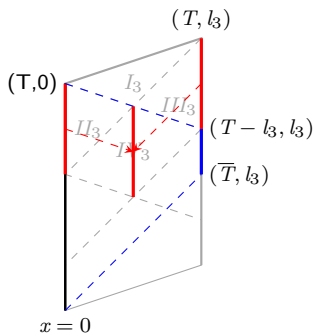
$$\vec{\phi} = (\phi^1(t, x), \phi^2(t, x), \phi^3(t, x)) \in C^0([0, T]; \bar{V}) \times C^1([0, T]; H),$$

where

$$\bar{V} = \left\{ \phi \in \prod_{i=1}^3 H^1(0, l_3) \mid \phi^1(0) = \phi^2(0) = \phi^3(0), \phi_x^1(l_1) = \phi_x^2(l_2) = 0 \right\} ..$$

- \implies At the ends $x = l_1$ and $x = l_2$ we get the traces of the solution $\phi^1(t, l_1), \phi^2(t, l_2) \in L^2(0, T)$.

Step3.2 (Estimation for ϕ^3):



It is easy to check that

$$\phi^3(t, x) = \begin{cases} 0, & (t, x) \in I_3, \\ \phi^3(t+x, 0), & (t, x) \in II_3, \\ \phi^3(t+l_3-x, l_3), & (t, x) \in III_3 \\ \phi^3(t+l_3-x, l_3) + \phi^3(t+x, 0), & (t, x) \in IV_3, \end{cases} \quad (23)$$

$$\|\varphi_3\|_{L^2(T-l_3, T)}^2 = \int_{T-l_3}^T \left[\phi^3\left(t - \frac{l_3}{2}, \frac{l_3}{2}\right) - \phi^3(t, 0) \right]^2 dt \quad (24)$$

$$\|\varphi_3\|_{L^2(\bar{T}, T-l_3)}^2 = \frac{1}{4} \int_{\bar{T}}^{T-l_3} \left(\phi^3(t+l_3, 0) + \phi^3(t-l_3, 0) + \int_{t-l_3}^{t+l_3} \phi_x^3(\tau, 0) d\tau \right)^2 dt \quad (25)$$

If $\bar{T} - l_3 > 0$, we get

$$\begin{aligned} \|\varphi_3\|_{L^2(\bar{T}, T)}^2 &\leq 6\|\phi^3(\cdot, 0)\|_{L^2(\bar{T}-l_3, T)}^2 + \int_{T-l_3}^T \left[\int_{t-l_3}^t \phi_x^3(\tau, 0) d\tau \right]^2 dt \\ &\quad + \frac{1}{2} \int_{\bar{T}}^{T-l_3} \left[\int_{t-l_3}^{t+l_3} \phi_x^3(\tau, 0) d\tau \right]^2 dt \\ &:= I_1 + I_2 + I_3 \end{aligned} \quad (26)$$

Moreover, in account of the transmission conditions at the adjoint node $x = 0$, we have

$$\begin{aligned} \phi^3(t, 0) &= \phi^1(t, 0) = \phi^2(t, 0), \\ -\phi_x^3(t, 0) &= \phi_x^1(t, 0) + \phi_x^2(t, 0), \end{aligned}$$

then

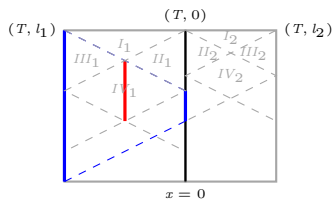
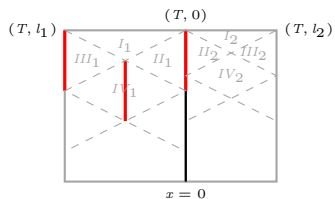
$$I_1 = 6\|\phi^i(\cdot, 0)\|_{L^2(\bar{T}-l_3, T)}^2, \quad i = 1, 2, \quad (27)$$

$$I_2 \leq 2 \sum_{i=1,2} \int_{T-l_3}^T \left[\int_{t-l_3}^t \phi_x^i(\tau, 0) d\tau \right]^2 dt, \quad (28)$$

$$I_3 \leq \sum_{i=1,2} \int_{\bar{T}}^{T-l_3} \left[\int_{t-l_3}^{t+l_3} \phi_x^i(\tau, 0) d\tau \right]^2 dt. \quad (29)$$

Step3.3 (Estimation for ϕ^i and ϕ_x^i , $i = 1, 2$):

(Step 3.3.1. Tools) Explicit Solution. Sidewise D'Alernbert Formula.



Step3.3 (Estimation for ϕ^i and ϕ_x^i , $i = 1, 2$):**(Step 3.3.1. Tools)** Explicit Solution. Sidewise D' Alernbert Formula.**(Step 3.3.2. Estimation for (27))**

$$\|\phi^1(\cdot, 0)\|_{L^2(\bar{T}-l_3, T)}^2 \leq 2\|\phi^1(\cdot, l_1)\|_{L^2(\bar{T}-l_3-l_1, T)}^2. \quad (30)$$

(Step 3.3.3. Estimation for (28))

$$\begin{aligned} \int_{T-l_3}^T \left(\int_{t-l_3}^t \phi_x^1(\tau, 0) d\tau \right)^2 dt &\leq c\|\phi^1(\cdot, l_1)\|_{L^2(T-l_1-2l_3, T)}^2 \\ &\leq c\|\phi^1(\cdot, l_1)\|_{L^2(\bar{T}-l_1-l_3, T)}^2. \end{aligned} \quad (31)$$

(Step 3.4. Estimation for (29))

$$\int_{\bar{T}}^{T-l_3} \left[\int_{t-l_3}^{t+l_3} \phi_x^1(\tau, 0) d\tau \right]^2 dt \leq c\|\phi^1(\cdot, l_1)\|_{L^2(\bar{T}-l_3-l_1, T)}^2. \quad (32)$$

The corresponding estimation for ϕ^2 is similar. Finally, substituting all estimations into (27)-(29), we get

$$\|\varphi_3\|_{L^2(\bar{T}, T)}^2 \leq c \left(\|\phi^1(\cdot, l_1)\|_{L^2(\bar{T}-l_3-l_1, T)}^2 + \|\phi^2(\cdot, l_2)\|_{L^2(\bar{T}-l_3-l_2, T)}^2 \right), \quad (33)$$

which implies the observability inequality (22) provided with $\bar{T} > l_3 + \max\{l_1, l_2\}$.

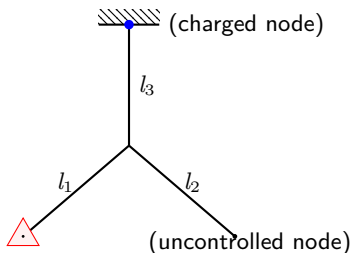
So far, we establish the duality between controllability and observability and prove the observability inequality (22), so we give a positive answer to the control problem as

Theorem 2.7 (Controllability)

Let

$$\bar{T} = l_3 + \max\{l_1, l_2\} \quad (34)$$

and $T > \bar{T}$. Then the control problem (9) is controllable of nodal profile at $x = l_3$ in time $t \in (\bar{T}, T)$.



$$\begin{aligned}
 x = l_3 : y^3(t, l_3) &= 0, & t \in (0, T), \\
 x = l_2 : y_x^2(t, l_2) &= 0, & t \in (0, T), \\
 x = l_1 : y_x^1(t, l_1) &= u^1(t), & t \in (0, T),
 \end{aligned} \tag{35}$$

Theorem 2.8

Let

$$\bar{T} = l_3 + l_1 \tag{36}$$

and $T > \bar{T}$. Then the system with (35) is controllable of nodal profile at $x = l_3$ in time $t \in (\bar{T}, T)$.

$$\boxed{
 \begin{aligned}
 \mathcal{F}_1 : L^2(0, T) &\longrightarrow L^2(\bar{T}, T) \\
 u^1 &\mapsto y_x^3(t, l_3)
 \end{aligned}
 } \tag{37}$$

proposition 2.9

Let $\bar{T} > l_3 + l_1$ and $T > \bar{T}$. There exists a constant $c > 0$, such that the observability inequality

$$\|\phi^1(\cdot, l_1)\|_{L^2(0, T)} \geq c \|\varphi_3(\cdot)\|_{L^2(\bar{T}, T)}, \forall \varphi_3 \in H_0^1(\bar{T}, T) \quad (38)$$

holds.

Key.

If we were able to prove that there exists $c > 0$ such that

$$\|\phi^1(\cdot, 0)\|_{L^2(\bar{T}-l_3, T)} \leq c \|\phi^1(\cdot, l_1)\|_{L^2(0, T)}, \quad (39)$$

$$\int_{T-l_3}^T \left[\int_{t-l_3}^t \phi_x^1(\tau, 0) d\tau \right]^2 dt + \int_{\bar{T}}^{T-l_3} \left[\int_{t-l_3}^{t+l_3} \phi_x^1(\tau, 0) d\tau \right]^2 dt \leq c \|\phi^1(\cdot, l_1)\|_{L^2(0, T)}^2, \quad (40)$$

and

$$\int_{T-l_3}^T \left[\int_{t-l_3}^t \phi_x^2(\tau, 0) d\tau \right]^2 dt + \int_{\bar{T}}^{T-l_3} \left[\int_{t-l_3}^{t+l_3} \phi_x^2(\tau, 0) d\tau \right]^2 dt \leq c \|\phi^1(\cdot, l_1)\|_{L^2(0, T)}^2, \quad (41)$$

we would obtain the observability inequality .

However, (41) does not obviously hold.

$$\int_a^b \left[\int_{t_1}^{t_2} \phi_x^2(\tau, 0) d\tau \right]^2 dt = \int_a^b \left[2\phi^2\left(\frac{t_1+t_2}{2}, \frac{t_2-t_1}{2}\right) - \phi^2(t_1, 0) - \phi^2(t_2, 0) \right]^2 dt \quad (42)$$

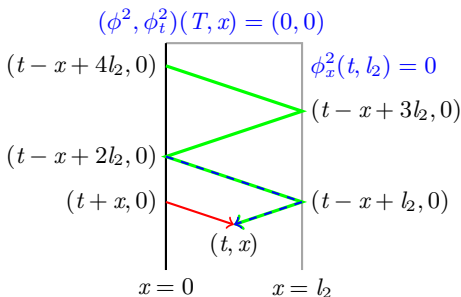


Figure: Waves going from $x = 0$ and reflecting at $x = l_2$

$$\phi^2\left(\frac{t_1+t_2}{2}, \frac{t_2-t_1}{2}\right) = \phi^2(t_2, 0) + \sum_{\{n \in \mathbb{N}^+ \mid t_1 + 2nl_2 \in [0, T]\}} \phi^2(t_1 + 2nl_2, 0). \quad (43)$$

$$\int_a^b \left[\int_{t_1}^{t_2} \phi_x^2(\tau, 0) d\tau \right]^2 dt \leq c \|\phi^2(\cdot, 0)\|_{L^2(t_1(a), t_2(b))}. \quad (44)$$

$$\begin{aligned}
& \int_{T-l_3}^T \left[\int_{t-l_3}^t \phi_x^2(\tau, 0) \, d\tau \right]^2 dt + \int_{\bar{T}}^{T-l_3} \left[\int_{t-l_3}^{t+l_3} \phi_x^2(\tau, 0) \, d\tau \right]^2 dt \\
& \leq c \|\phi^2(\cdot, 0)\|_{L^2(T-2l_3, T)}^2 + c \|\phi^2(\cdot, 0)\|_{L^2(\bar{T}-l_3, T)}^2 \\
& \leq c \|\phi^1(\cdot, 0)\|_{L^2(\bar{T}-l_3, T)}^2 \\
& \leq c \|\phi^1(\cdot, l_1)\|_{L^2(\bar{T}-l_3-l_1, T)}^2,
\end{aligned} \tag{45}$$

where the constants c are different from line to line. The third inequality (41) is proved.

In summary, the observability inequality (38) holds provide with $\bar{T} - l_3 - l_1 > 0$. □.

Nodal Control Problem. (to do).

- Optimal L^2 control. HUM control(J.-L.-Lions 1988).
- Nonlinear Case. Lack of duality. (Implicit duality¹². Exact Observability Problem for quasilinear hyperbolic problem.)

¹²Tatsien Li. Controllability and Observability for Quasilinear Hyperbolic Systems. 2010.

Thanks.