

# Discovering scaling laws for heat transport using convex optimization

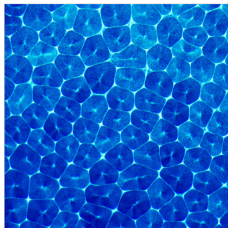
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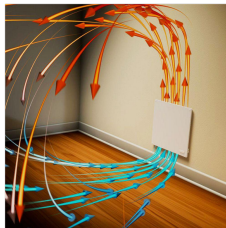
Joint work with:

Ali Arslan, John Craske, Andy Wynn (*Imperial College*)  
Anuj Kumar (*UC Santa Cruz*)

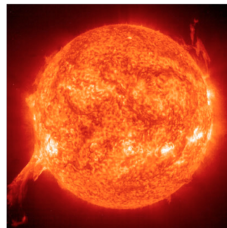
# Why heat transport?



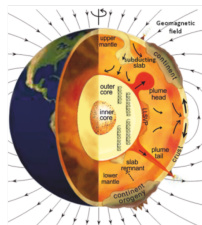
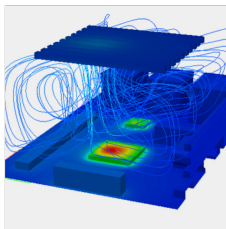
Surface tension



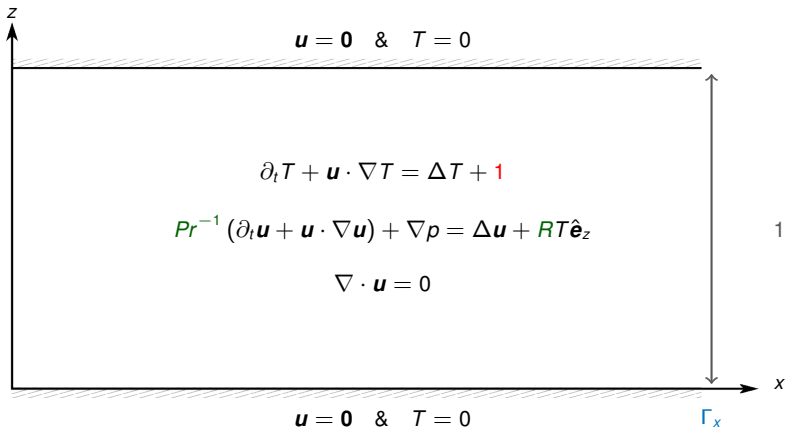
Boundary-driven



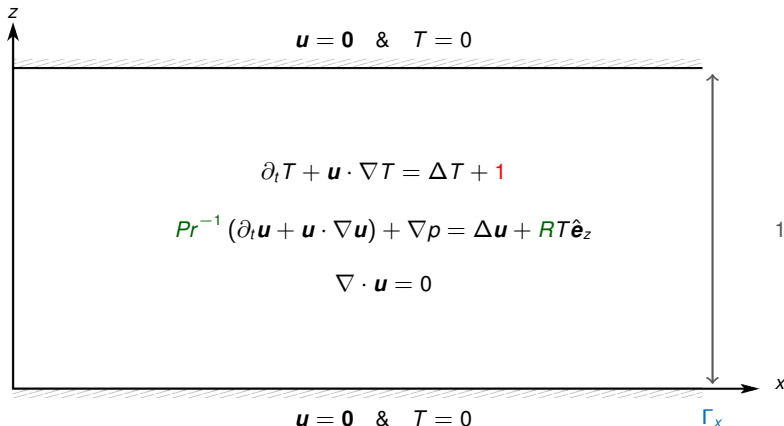
Internal heating



# A periodic layer with cool and sticky boundaries



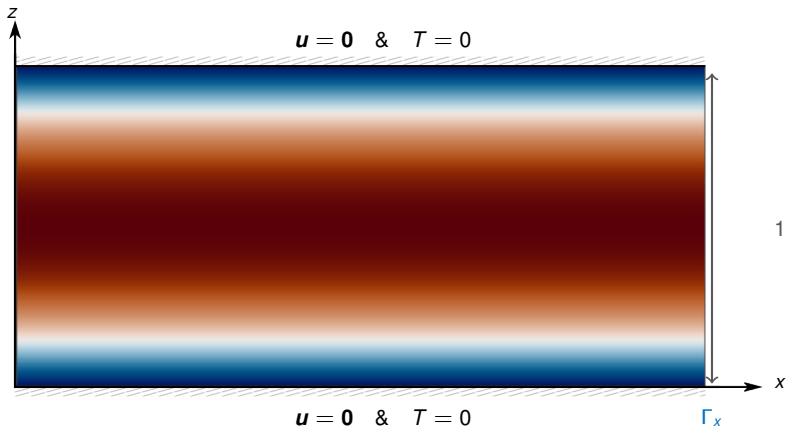
# A periodic layer with cool and sticky boundaries



Which fraction of the heat input exists through the top vs the bottom?  
How do these fractions depend on  $R$  (heating strength) and  $Pr$  (fluid's inertia)?



## Weak heating (small $R$ ) = no flow



$$\mathcal{F}_{\text{top}} = \frac{1}{2} \quad \mathcal{F}_{\text{bot}} = \frac{1}{2} (= 1 - \mathcal{F}_{\text{top}})$$

# Strong heating (large $R$ ) = turbulence

Video courtesy of John Craske

$$\mathcal{F}_{\text{top}} > \frac{1}{2}$$

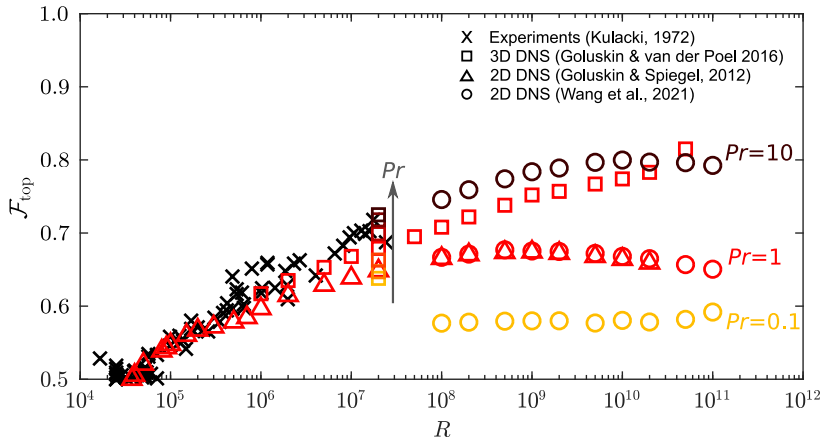
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$$\mathcal{F}_{\text{top}} > \frac{1}{2}$$

**Theorem (Goluskin & Spiegel, 2012):**  $\frac{1}{2} \leq \mathcal{F}_{\text{top}} \leq 1$  independently of  $R$  and  $Pr$ .

# Simulations tell a different story!



# Plan for today

1. Estimating  $\mathcal{F}_{\text{top}}$  via infinite-dimensional convex optimization
2. Results from numerical approximation
3. From numerics to proofs
4. Extensions and open problems (depending on time!)

# Basic identities

$$\mathcal{F}_{\text{top}} = \frac{1}{2} + \frac{1}{R} \overline{\langle |\nabla \mathbf{u}|^2 \rangle} \quad \sim \text{kinetic energy dissipation}$$

Notation:

- $w$  = vertical velocity of the fluid
- $T$  = temperature
- $\langle \cdot \rangle$  = space average
- $\overline{\cdot}$  = infinite-time average

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**Question:** Can we prove that

$$\overline{\langle wT \rangle} \leq \frac{1}{2} - f(R, Pr)$$

for some positive function  $f$ ?



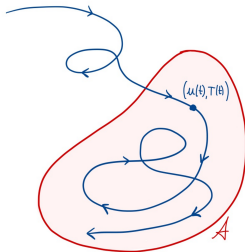
# Bounding time averages

**Observation:** If  $\mathcal{V}\{\mathbf{u}, T\}$  remains uniformly bounded along solutions,

$$\overline{\frac{d}{dt}\mathcal{V}\{\mathbf{u}(t), T(t)\}} = \limsup_{t \rightarrow \infty} \frac{\mathcal{V}\{\mathbf{u}(t), T(t)\} - \mathcal{V}\{\mathbf{u}_0, T_0\}}{t} = 0$$

Then,

$$\begin{aligned} \overline{\langle \mathbf{w}(t)T(t) \rangle} &= \overline{\langle \mathbf{w}(t)T(t) \rangle + \frac{d}{dt}\mathcal{V}\{\mathbf{u}(t), T(t)\}} \\ &= \overline{\langle \mathbf{w}(t)T(t) \rangle + \mathcal{L}\mathcal{V}\{\mathbf{u}(t), T(t)\}} \\ &\leq \inf_{\mathbf{v}} \sup_{(\mathbf{u}, T) \in \mathcal{A}} \left\{ \langle \mathbf{w}T \rangle + \mathcal{L}\mathcal{V}\{\mathbf{u}, T\} \right\} \end{aligned}$$



Tobasco et al (2018) + Rosa & Temam (2020): The strategy is **sharp** for well-posed ODEs/PDEs with **compact** absorbing sets.

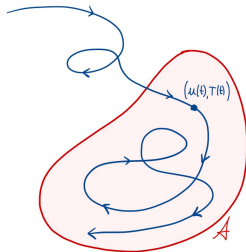
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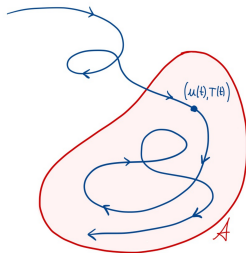
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**How should one choose  $\mathcal{V}$ ?**

# The Doering & Constantin way (1994+)

Consider

$$\mathcal{V}\{\mathbf{u}, T\} = \frac{\beta_1}{2PrR} \langle |\mathbf{u}|^2 \rangle + \frac{\beta_2}{2} \langle |T - \varphi(z)|^2 \rangle$$

where

$$\varphi(0) = 0 \quad \varphi(1) = 0$$

Then,

$$\begin{aligned} \langle wT \rangle + \mathcal{L}\mathcal{V}\{\mathbf{u}, T\} &= \frac{1}{2} - \langle \tau(z) \rangle \\ &\quad - \langle [\tau'(z) + 1 + \beta_2 z] T_z \rangle \\ &\quad - \langle \beta_1 R^{-1} |\nabla \mathbf{u}|^2 + \beta_2 |\nabla T|^2 + [\tau'(z) - \beta_1] wT \rangle \end{aligned}$$

Maximize over the absorbing set  $\mathcal{A}$  defined using

- ▶ Boundary conditions
- ▶ Incompressibility:  $\nabla \cdot \mathbf{u} = 0$
- ▶ **Minimum principle:** at long times,  $T \geq 0$  almost everywhere in the fluid domain  
 $\rightsquigarrow$  introduce a “Lagrange multiplier”  $\lambda(z)$

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# An explicit convex optimization problem

The mean vertical convective heat flux satisfies

$$\overline{\langle wT \rangle} \leq \frac{1}{2} - \int_0^1 \tau(z) \, dz + \frac{1}{4\beta_2} \int_0^1 |\tau'(z) - \lambda(z) + \beta_2 z - \frac{1}{2}\beta_2|^2 \, dz$$

provided that

$$\tau(0) = 1$$

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$\lambda$  is non-decreasing

and, for all  $\mathbf{u}$  and  $T$  satisfying  $\nabla \cdot \mathbf{u} = 0$  and the flow's boundary condition,

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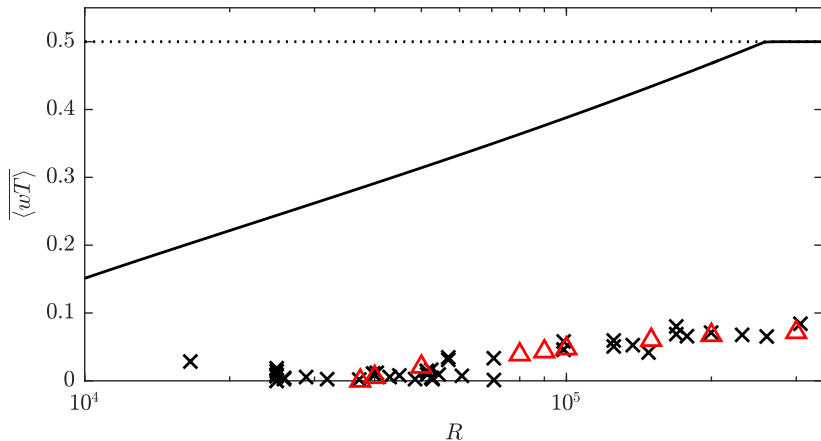
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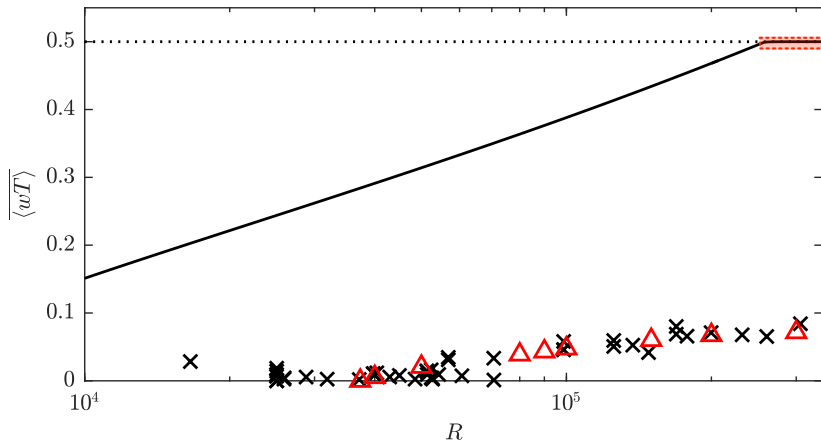
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# Numerically optimized bounds

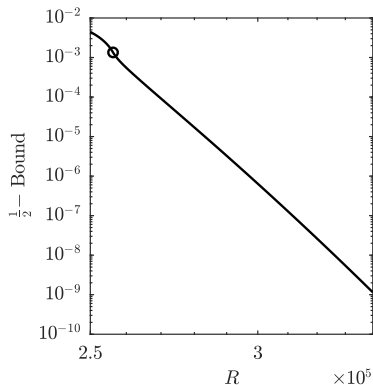
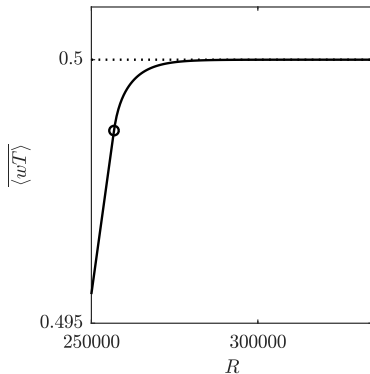




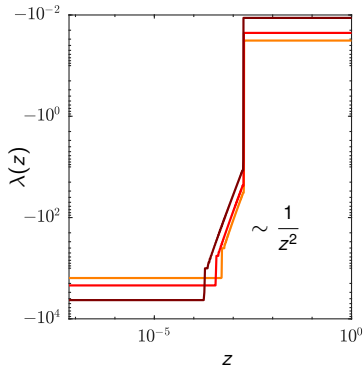
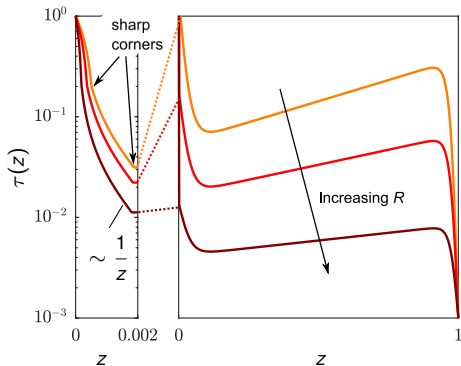
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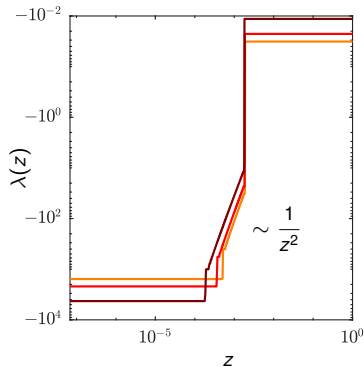
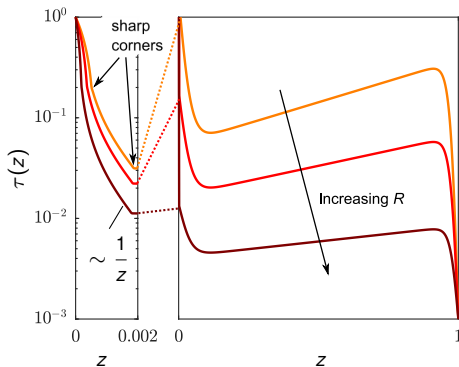
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# Optimizers

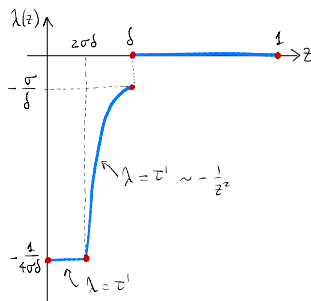
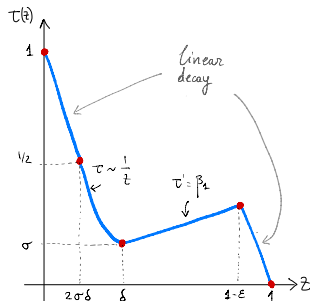


# Optimizers



$$\tau'(z) \approx \lambda(z) \text{ near } z = 0$$

# Turning numerical results into rigorous proofs



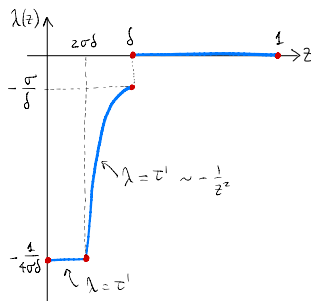
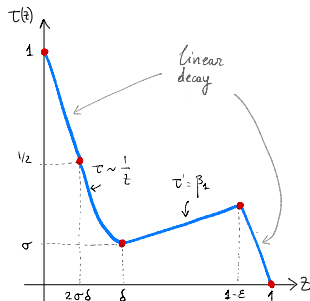
$$\overline{\langle wT \rangle} \leq \frac{1}{2} - \sigma\delta \ln\left(\frac{1}{\sigma}\right) + O(\sigma\delta R^{\frac{3}{5}})$$

provided that

$$\langle \beta_1 R^{-1} |\nabla \mathbf{u}|^2 + \beta_2 |\nabla T|^2 + [\tau'(z) - \beta_1] wT \rangle \geq 0$$

Key estimate:  $\langle (z + \sigma\delta)^{-2} wT \rangle \lesssim \langle |\nabla \mathbf{u}|^2 + |\nabla T|^2 \rangle$

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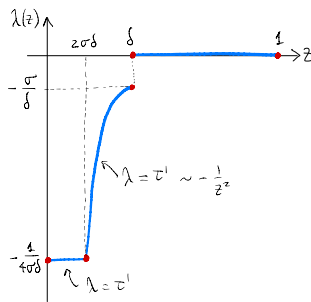
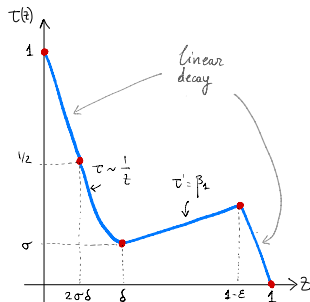
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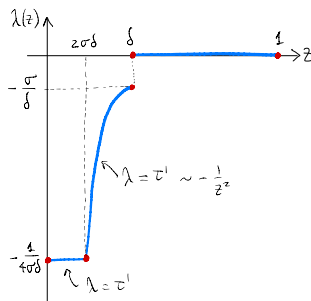
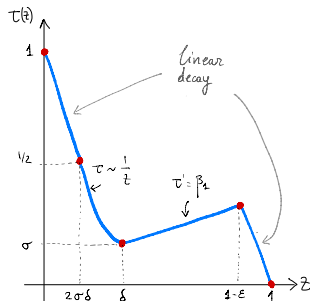


Theorem (Kumar, Arslan, F, Craske, Wynn, JFM2021)

There exist positive constants  $c_1$  and  $c_2$  such that, for any value of  $Pr$  and sufficiently large  $R$ ,

$$\overline{\langle wT \rangle} \leq \frac{1}{2} - c_1 R^{\frac{1}{5}} \exp\left(-c_2 R^{\frac{3}{5}}\right)$$

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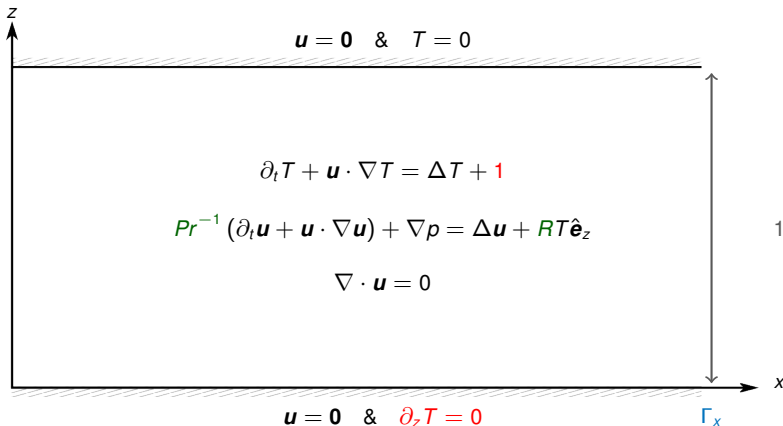
There exist positive constants  $c_1$  and  $c_2$  such that, for any value of  $Pr$  and sufficiently large  $R$ ,

$$\mathcal{F}_{top} \leq 1 - c_1 R^{\frac{1}{5}} \exp\left(-c_2 R^{\frac{3}{5}}\right)$$



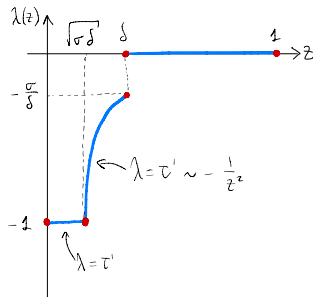
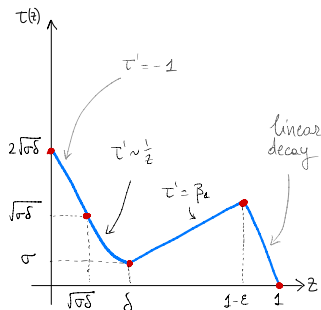
# **Extensions**

## Extension 1: Insulating bottom boundary



$$\overline{\langle wT \rangle} = R^{-1} \overline{\langle |\nabla \mathbf{u}|^2 \rangle} \sim \text{mean dissipation of kinetic energy}$$

## Similar result, different exponent

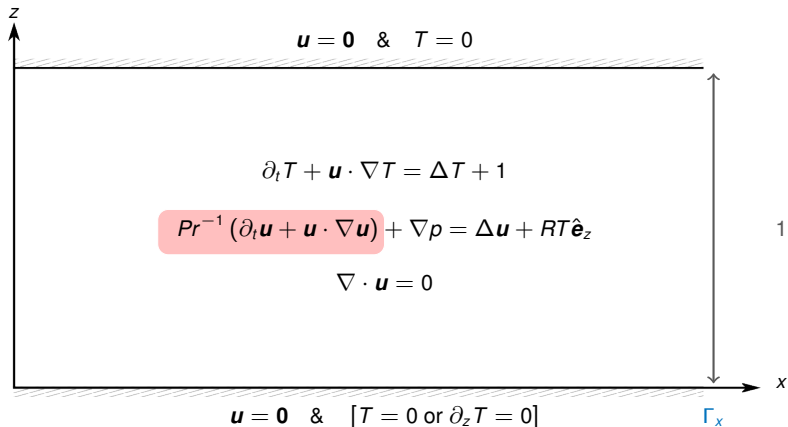


Theorem (Kumar, Arslan, F, Craske, Wynn, JFM2021)

There exist positive constants  $c_1$  and  $c_2$  such that, for any value of  $Pr$  and sufficiently large  $R$ ,

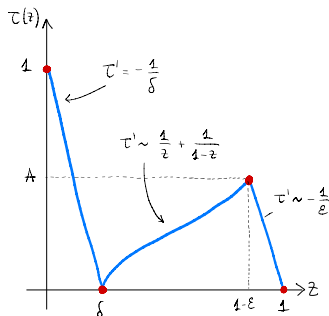
$$\overline{\langle wT \rangle} \leq \frac{1}{2} - c_1 R^{-\frac{1}{5}} \exp\left(-c_2 R^{\frac{3}{5}}\right)$$

## Extension 2: “Thick” fluids with $Pr = \infty$



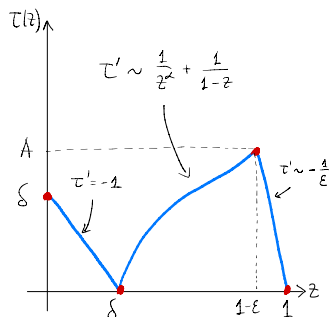
# Much better bounds!<sup>1</sup>

Cool bottom ( $T = 0$ )



**Theorem:**  $\overline{\langle wT \rangle} \leq \frac{1}{2} - cR^{-2}$

Insulating bottom ( $\partial_z T = 0$ )



**Theorem:**  $\overline{\langle wT \rangle} \leq \frac{1}{2} - cR^{-4}$

<sup>1</sup> Arslan, F, Craske & Wynn, [arXiv:2205.03175](https://arxiv.org/abs/2205.03175) (2022)

# Summary

Model	Arbitrary fluids	“Thick” fluids ( $Pr = \infty$ )
$\overline{T = 0}$		
$\overline{T = 0}$	$\overline{\langle wT \rangle} \leq \frac{1}{2} - c_1 R^{\frac{1}{5}} e^{-c_2 R^{\frac{3}{5}}}$	$\overline{\langle wT \rangle} \leq \frac{1}{2} - cR^{-2}$
$\overline{T = 0}$		
$\overline{\partial_z T = 0}$	$\overline{\langle wT \rangle} \leq \frac{1}{2} - c_1 R^{-\frac{1}{5}} e^{-c_2 R^{\frac{3}{5}}}$	$\overline{\langle wT \rangle} \leq \frac{1}{2} - cR^{-4}$

However:

Are the constructions leading to these bounds **optimal**?

Are the bounds **sharp** for convective flows?

Which flows optimize  $\overline{\langle wT \rangle}$ ? Are they perhaps **steady**?

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$T = 0$	$\overline{\langle wT \rangle} \leq \frac{1}{2} - c_1 R^{\frac{1}{5}} e^{-c_2 R^{\frac{3}{5}}}$	$\overline{\langle wT \rangle} \leq \frac{1}{2} - cR^{-2}$
$T = 0$		
$T = 0$		
$\partial_z T = 0$	$\overline{\langle wT \rangle} \leq \frac{1}{2} - c_1 R^{-\frac{1}{5}} e^{-c_2 R^{\frac{3}{5}}}$	$\overline{\langle wT \rangle} \leq \frac{1}{2} - cR^{-4}$

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